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ELEVENTH AND TWELFTH PROGRESS REPORT

ON

MANUFACTURING METHODS AND TECHNIQUES FOR MINIATURE HIGH VOLTAGE HYBRID MULTIPLIER MODULE

CONTRACT NO. DAABO7-76-C-0041



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Generation Image Intensifier Tubes, High Voltage Recti	itiers, Ceramic Capacitor Banks
Miniature Modules.	
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ELEVENTH QUARTERLY PROGRESS REPORT

MANUFACTURING METHODS AND TECHNIQUES FOR MINIATURE HIGH VOLTAGE HYBRID MULTIPLIER MODULES

CONTRACT NO. DAABO7 - 76 - C - 0041

PREPARED BY: M. I. MATUSZEWSKI, P.ENG.

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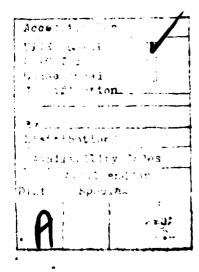
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PURPOSE

This Contract covers component designs, mounting and interconnection techniques, tooling and test methods and other
manufacturing methods and techniques required for production
of rectangular and curved miniature high voltage multiplier
modules. These units are to be used in low cost power
supplies for image intensifier tubes. The full scope and
details of the specification are given in Appendix A to the
Eighth Quarterly Report.

Major milestones in this program consist of delivery of the following items:

- (1) First and second engineering samples and test data. '
- (2) Production line layout and schedule.
- (3) Confirmatory samples and test data.
- (4) Production line set-up.
- (5) Pilot production run.
- (6) Production rate demonstration.
- (7) Preparation and publication of a final report.

The general approach is to design and set-up a cost-effective production capability, utilizing already established device technologies and materials, and to demonstrate the production line capability to fabricate at the rate of 125 acceptable units per 40 hour week.

1. INTRODUCTION

This report describes briefly the progress in the Manufacturing Methods and Techniques for Miniature High Voltage Hybrid Multiplier Modules Program, made during the latest calendar **year**

In the First Quarterly Report the design and the manufacturing process for rectangular and curved multiplier modules were described. Prototype rectifier-substrate assemblies were fabricated and then redesigned to simplify the assembly operation. The specification covering the requirements for the multiplier modules forms Appendix A of the Report.

In the Second Quarterly Report results of the electrical evaluation of the first sample batch of rectangular capacitor banks TSK 25-250 and TSK 25-251 were given, the choice of the rectifier was made and electrical test results were presented on non-modular multipliers fabricated with TSK 25-250 and TSK 25-251 capacitor banks and standard HV2OPD four-junction rectifiers, to evaluate these components.

In the Third Quarterly Report results of electrical tests on rectangular multiplier modules were presented.

For an input voltage of 1 KV, efficiencies above 96% under no-load conditions and above 95% with 500 nA load currents were achieved for all multipliers assembled with TSK 25-250 and TSK 25-251 and three-chip rectifiers. Low ripple voltages, input capacitances and charging currents were also measured on these multipliers.

Results of the mechanical and electrical evaluation of TSK 25-249 curved capacitor banks were also presented in the Third Quarterly Report.

In the Fourth Quarterly Report work on impregnation and coating of the multipliers was discussed as well as some problems associated with the fabrication of the rectifier-substrate assemblies. The fabrication of rectangular and curved multipliers for the First Engineering Sample was discussed.

In the Fifth Quarterly Report were presented the results of electrical performance testing at the room, high $(+52^{\circ}\text{C})$ and low (-54°C) temperatures, as well as effects of thermal shock, and high and low temperature storage.

In the Sixth and Seventh Quarterly Reports were presented the results of testing of rectangular and curved multipliers to the Second Engineering Sample requirements,

steps to improve the frequency performance of the multipliers and optimization of the rectifiers for these devices, as well as results of life testing of multipliers.

In the Eighth Quarterly Report the results of the reliability testing of rectangular and curved multipliers to the Second Engineering Sample requirements were analyzed and further steps to improve the performance of the multipliers and optimize the rectifiers for these devices were discussed.

In the Ninth Quarterly Report the results of further life testing of rectangular and curved multipliers was discussed. The commencement of the Confirmatory Sample phase was described including improvements in the manufacturing methods.

In the Tenth Quarterly Report a data was presented on material and fixtures used in the fabrication of the multiplier modules.

The technique of silk screening the conductive epoxy onto the components is described in fabrication of the voltage multipliers.

...3

FABRICATION AND EVALUATION OF MULTIPLIERS

During the first quarter of 1979 most of the work was devoted to manufacturing and assembling of the multiplier.

modules which were described in the Tenth Quarterly Report.

In January the vacuum fixture for molding parts for the silk-screening process has been built. Additional screens had been received from ERIE, PA.

However, when production started on the 10 curved multipliers, 7 were "open", 1 was "shorted" and the other 2 indicated a short of several rectifiers within the diodechain. In February, 11 pieces were assembled, 3 were good on VF (forward voltage drop), 1 was good on V_0 (optional test), 2 broke physically in assembly, 6 were "open" when tested on VF.

At the time of writing this report, the reject units could not be located to do a reject analysis, but subsequent recommendations by previous program manager were requested and on file.

...4

Most of the March was spent on the design and fabrication of fixtures and tooling for the assembly of capacitors to substrates and for the soldering of leads to capacitors. The Ceramic Engineering Group provided us with another 23 tapped capacitors. They have been informed of the problem of the oversize capacitors and they assured me to be able to supply capacitors that are 80° in arc.

In June 1979, it became obvious that we could not fabricate the parts on any production scale using previous method and design. A new assmebly technique was developed and is outlined below.

The same rectifiers were used as before, an additional epoxy roll-coat were given and leads were retained to assure good solder connections. The capacitor is notched to make room for a diode body.

The same thickness of ceramic is retained in order to maintain a sufficiently high voltage breakdown.

The modified assembly is illustrated in an isometric sketch TSF-31.-112. The new method, as a simplification of original concept, should give cost saving in large scale production. With regards to the change, the following modifications were requested:

. . . 5

1) Part II Section II, Suppliers Schedule Date - The schedule to be changed to the following:

Item No. 0001AB - Confirmatory Sample

Delivery: 4 February 1980

Item No. 0001AC - Pilot Run

Delivery: 16 June 1980

Item No. B003 - Test Report of Confirmatory Samples

Delivery: 4 February 1980

Item No. C003 - Final Report

Delivery: Draft due 14 July 1980 (First distribution 30

days after approval.)

Item No. COO4 - General Report, Step 11

Delivery: 30 days after approval of First Report.

Item No. 0005AA - Rehability Testing

Delivery: 16 June 1980

- 2) Electronics Command Technical Requirements SCS-495.
- a) On pages 20 and 21, para 2.1 on each page to be changed to following:
- "2.1 Di and D $_{0}$ leads: 0.015 Diameter silver or tinned copper."
- b) On pages 20 and 21, AC and GND leads to exit the package on the same face as the $D_{\rm i}$ lead (as illustrated in sketch TSK 312-112)

The schedule changes result from the delivery of the new capacitors by our vendor. The reason for request 2(a), is simple - we intend to use the diode's own lead for D_i and D_o and its diameter is .015". Regarding the change in lead positions, this is necessitated by the fact that the leads can no longer emerge from the sides as there would be too great a probability of breakdown from the leads to the diodes nearest them. Therefore, the only feasible alternative is the one suggested above and any testing on such parts must be performed in a dielectric fluid or after further encapsulating the entire multiplier.

CONCLUSION

Nearly every position within this contract has changed many times in 1976, 1977 and 1978. For example: the Procuring Contracting Officer at Fort Monmouth was changed 3 times, the Contracting Officer's Technical Representative 2 times, the Project Engineer at Fort Belvoir 3 times, the Representative for Canadian Commercial Corporation 3 times.

Finally, the ERIE Programme Manager was initially A. Kennedy, then Dr. M. Korwin Pawlowski (Warch /7), B. G. Gordon (September 1978) and as of January 1980 M. Matuszewski.

These changes have negative impact in continuation of the project as for delivery schedule. However, additional effort will be made by present Programme Manager to fulfill our commitments.

Program for first quarter of 1980:

- 4.1 Most attention must be placed to keep progress according to schedule.
- 4.2 Necessary changes in design to assure production assembly should be made. Present design proposition is not practical to mass assembly.
- 4.3 Initiate manufacture of the proper capacitors.
- 4.4 Design and fabricate tools and jigs.
- 4.5 Fabricate and test engineering sample.

PUBLICATIONS AND REPORTS

No reports or publications were made on the work associated with this program during the last year.

IDENTIFICATION OF PERSONNEL

Brief descriptions of the background of technical personnel involved were included in the preceding Progress Reports.

The following persons worked in their area of responsibility:

INDIVIDUAL	RESPONSIBILITY	HRS.
B. G. Gordon	Programme Manager	484
J. Pack	Manufacturing Personnel	366
R. Shah	Programme Manager	80
K. Cram	Draughtsman	13
V. Glenn	Q.C. Inspector	15
B. Heidt	Process Engineering Supervisor	112.1
P. Maples	Senior Engineering Technician	306.8
D. Regan	Senion Engineering Technician	48.5
F. Treverton	Senion Test Technician	1
TOTAL HO	OURS - in 1979	1441.4
TOTAL HO	OURS - to date	6295.4

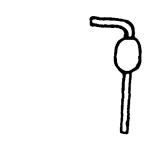
METHOD OF ASSEMBLY, AS USED ON THE

PROTOTYPE DUMMY SAMPLES

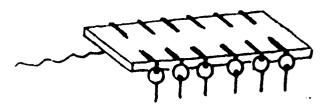
1. Solder input wire to common side of ? capacitors.



Pre-cut and bend 12 diodes (6 cathode to bend, 6 anode ro bend,)



3. Solder 12 diodes to the first capacitor.



4. Locate second capacitor. Bend 12 Diode leads, solder to second capacitor



Solder 2 output leads to second capacitor.



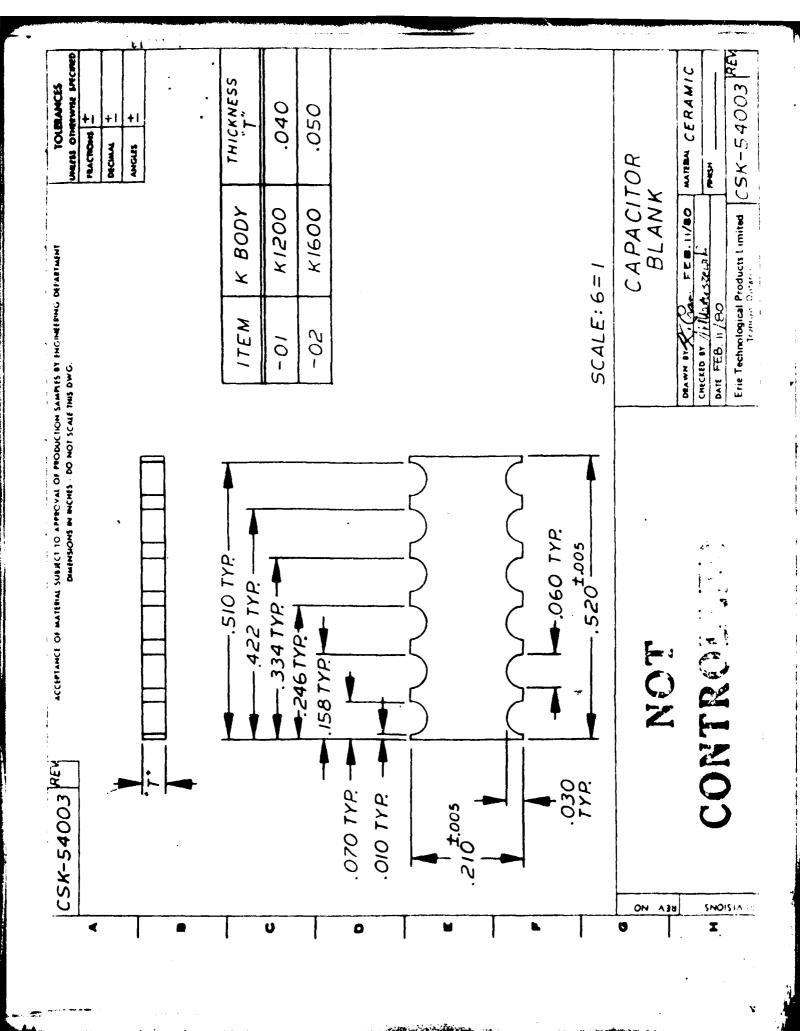
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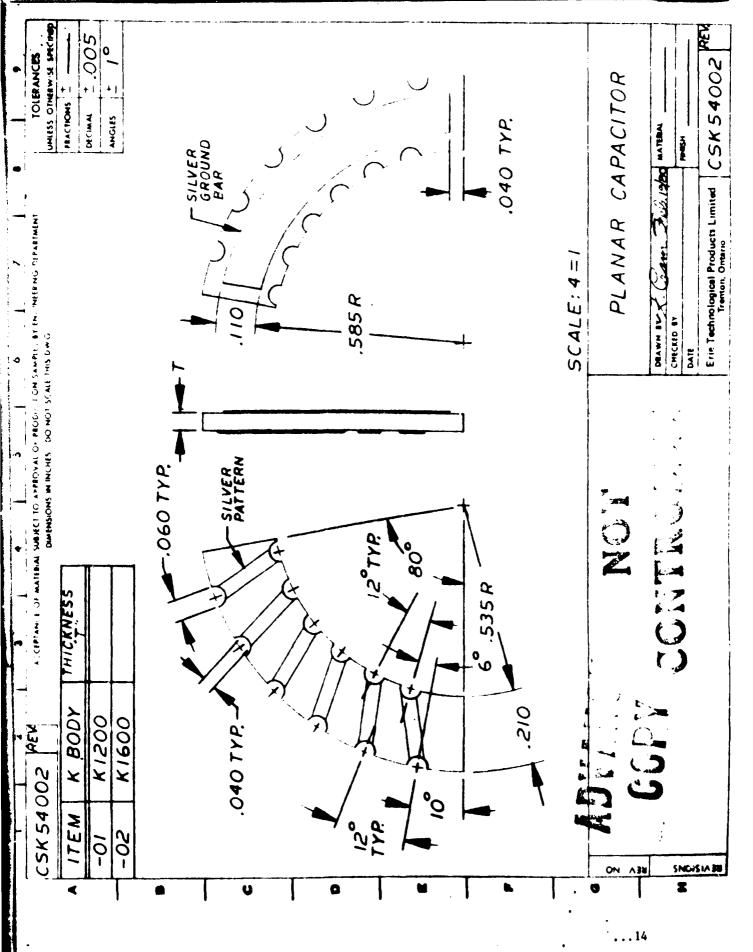
Erie Technological Product

Erie Technological Products of Canada Ltd. Trenton, Ontario

TSK-312-112







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K.I. SEMY		DAAB07 - 76 - C - 0041
9 PERFORMING ORGANIZATION NAME AND ADDRESS Erie Technological Products of Canado 5 Fraser Avenue TRENTON, Ontario, Canada K8V 55	·	10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS Project No. 2769766
U. S. Army ERADCOM, Night Vision Optical Laboratories Fort Belvoir, VA 22060 14 MONITORING AGENCY NAME & ADDRESS(II dillerent		2nd Feb. 1982 13. NUMBER OF PAGES 22
14 MONITORING AGENCY NAME & ADDRESS(II dillorent	from Controlling Office)	UNCLASSIFIED 15a. DECLASSIFICATION DOWNGRADING SCHEDULE
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TWELFTH QUARTERLY REPORT QUARTERLY PROGRESS REPORT THIRD QUARTER 1981

MANUFACTURING METHODS AND TECHNIQUES FOR MINIATURE HIGH VOLTAGE HYBRID MULTIPLIER MODULES

CONTRACT NO. DAABO7 - 76 - C - 0041

PREPARED BY: K.I. SEMY

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In the Tenth Quarterly Report a data was presented on material and fixtures used in the fabrication of the multiplier modules.

The technique of silk screening the conductive epoxy onto the components is described in fabrication of the voltage multipliers.

In the Eleventh Report, fabrication and evaluation of the multiplier was discussed with notched capacitors and P-package diodes from Murata Erie North America, Inc.

ASSEMBLY OF MULTIPLIER (MIREK MATUZEWSKI PROCESS)

- Dip silvered ceramic capacitors into 60% lead 40% tin solder solution.
- 2. Solder silver strip to the ground pattern on ceramic as shown on figure 1.

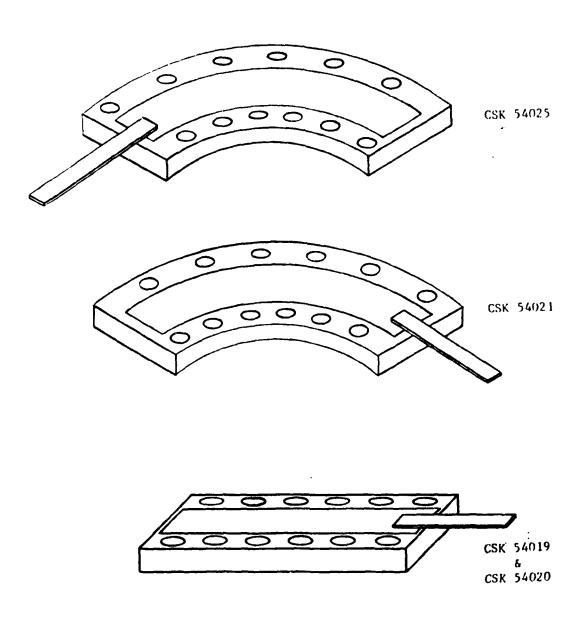
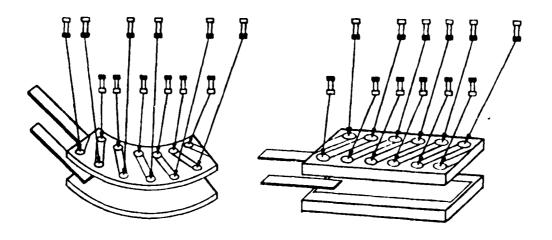


Fig. 1 Position of "ground" terminals.

- 3. Place capacitors in the assembly fixture.
- 4. Locate diodes in holes in ceramic capacitors with the orientation as shown on figure 2a and 2b



(a)

Fig. 2. Diode assembly module.

- (b)
- a) TSK 313-113 module b) TSK 312-114
- 5. Apply flux and solder to create bridges between ceramic silvered pattern and diodes.
- 6. Attach silver lead terminals to the input and output of the multiplier.
- 7. Etch devices for 1 minute, clean in ultrasonic and D.I. water.
- 8. Dip devices into varnish and cure in 160°C for 24 hours.
- 9. Place device in the rubber mold and fill it with epoxy coating.
- 10. Cure epoxy in 160°C for 12 hours.
- 11. Remove multiplier from rubber mould.

PROBLEMS

- Extensive cracking of the capacitor during solder dipping operation.
- 2. The surface damage on the diodes caused by the sawing of the stack was removed after assembly of the multiplier. Assuming 90% test yield on the diode, the overall yield to complete multipliers would be very small as one diode in any 12 diodes used in the multiplier could reject the complete multiplier assembly.
- 3. During the soldering operation it is difficult to control the size, as a solder bridge had to be formed between the diode and the silver of the ceramic with the solder. This could only be achieved by using large amount of solder. Hence the overall thickness of the multiplier was typically 0-200" to 0-220". The diode had to be subsequently lapped down to size which resulted in some yield loss.
- 4. The hand soldering operation gives us limited output.

After the departure of Mirek Matuszewski the project responsibilities were assumed by the writer, and therefore actions were taken to modify the process.

The following process changes were made:

- 1. The diodes used for assembly were etched, varnished, epoxy coated and 100% tested before assembly of multiplier.
- 2. The overall diameter of the diode had to be maintained to be less than diameter of the hole in the ceramic capacitors. In December 1980, we started soldering multipliers and after eliminating assembly rejects we produced approximately 33 pcs. of TSK 312-000 and 30 pcs of TSK 313-000 to meet the confirmatory sample requirements.

RESULTS:

The multipliers were tested for Cr. 1 test and results are as below.

	No. of Pieces to Test	Good Pieces	Charging Current reject	Efficiency Reject
TSK 312-00	30	20	6	6
TSK 313-00	30	16	7	7
Yield on test	TSK 312-00	60.6%		
	TSK 313-00	53.3%		

The multipliers passing test were showing charging current of 200 to 250 microamps. It was therefore decided to initiate further optimisation of the diode and the capacitor. (Test results pg. 11)

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3		955	5.710	45.2 4.2	. 0.3	320	7.13		
9	5	95.2	5.690	94.8	7.0	. 200	21.9		
		957	5720	953	20	230	2.10		
ر ا ا	•	95.7	5.710	95.2	0.5	380	649		
€ •	~··	7.56	5.690	9.46	0	. 250	6.10		
0	ARC	الح	1	ĺ		1			
= -	5.740	95.7	5,720	953	0.1	130	£99		
ン	5.360	89.3	4.860	31.0	دي دي	160	6.33		
	3 5.310	83.5	5.260.	82.7	ზ 0	200	5.47		
ν c		756	5.710	95. L	. 0.5	220	6.24		
2 -	5.410	40.7	5.630	84.3	6.0	130	6.35		
9	-	955	5.700	95.0	'S'	730	6.53		
	+	95.7	5200	95.2	0.5	220	84.9		
	011.5	45,2	5.690	ر ا ا	1.0	300	6.50	•	j
	+		. 5.720	45.3	H0 .	. 400	6.36	•	1
	5.740	45.7	5710	て <u>3</u> 5	0.5	340	**·9	-	!
	+	95.7	5.7.30	953	0	330	9.79		
	1	26.3	5,000	7.98	<u>.</u>	081	5.77		,
	57	. 953	5.700	950	6.3	. 220	7.00		,
- 24	5730	95.5	. 5.700.	45.0	0.5	350	. 849	!	
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PRODUCTS	_
TECHNOCOGICAL	CH CANADA TTO
ERIE TECH	

					Ŭ L C	CANADA, LTD				
SHEET	1 40 T		00.1.1	OUALITY CONTI	TROL DEPT.	ı	ORDED DA	RECORDED DATA SHEET	· ·	
P. D.	7465: Bo7.36-C-004/	.	TEST FORT MODIMOUTH CONFIRMATORY PART 154, 919/ 5/100 Const	Journaut.	TH CONFIRMAT	1	Testine M.IT M	TESTING (GROUP I)		
,TY			SPECIAL DETAILS	ع ر د ا	Spic. 12	50			A, proceed By	
TEST DATE TEST COND. PARAMETER ZUPUT VOLT LOAD CLARENT SPEC. PARAME	Mussicati Jose 2p/p C 6 2n B 6 2n B	20	South CA	CACCUCATEDA Se COME SOOM 2	BEFF.	CHG CURES 1000 / P = 2 m A = 3.1.3	''	Luhr CAP. 1000 Uplp -27 A 3 2 1.2		
REPOSE MENT	KVK	9490 mm	KAC	6	d 2 Comas	250 y A 1005		8 pc. max.		
Black 23 5	5740 5720 5730 9 5140 5440 5130	45.7 45.3 44.3 41.5 45.2 45.5	5.720 5.690 5.670 5.470 5.470 5.80	98.3 98.3 88.3 88.3 88.3	7,000000	330 320 320 250 450		6.93 6.63 6.24 5.80 5.80		
138WTN										
רשבצעט		:		(
CASTWIG!						,				
			•					1 1		

PLANS

- 1. Evaluate reduced capacitance.
- 2. Decrease reverse recovery time of diode.
- 3. Improve assembly process, automate soldering to increase throughput and yield.

CONCLUSION:

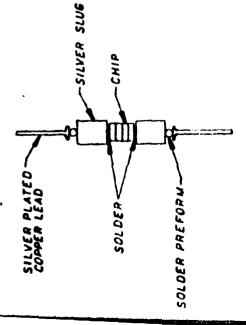
As reported in the eleventh quarterly report every position in the contract has changed many times. We have to report once again that Mirek Matuszewski who has been the Program Manager since January, 1980 left the company and his project responsibilities have been taken over by the writer. We are making a concentrated effort to complete this project and have also recruited one full time operator for fabrication of confirmatory samples and pilot production run.

We have requested for a change in schedule for delivery of samples and it shall be reported in my next quarterly report.

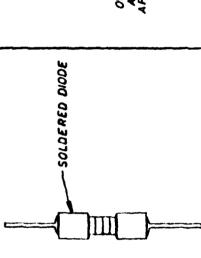
PUTLICATION & REPORT

No publications and reports have been issued in this quarter.

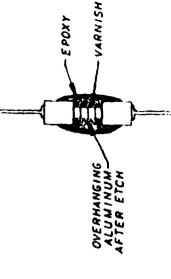
STEP ! ASSEMBLY IN JIG



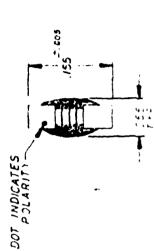
FURNACE SOLDERING IN ASSEMBLY JIG STEP 2



STEP 3 DIODE ETCHED, VARNISHED, *EPOXY COATED



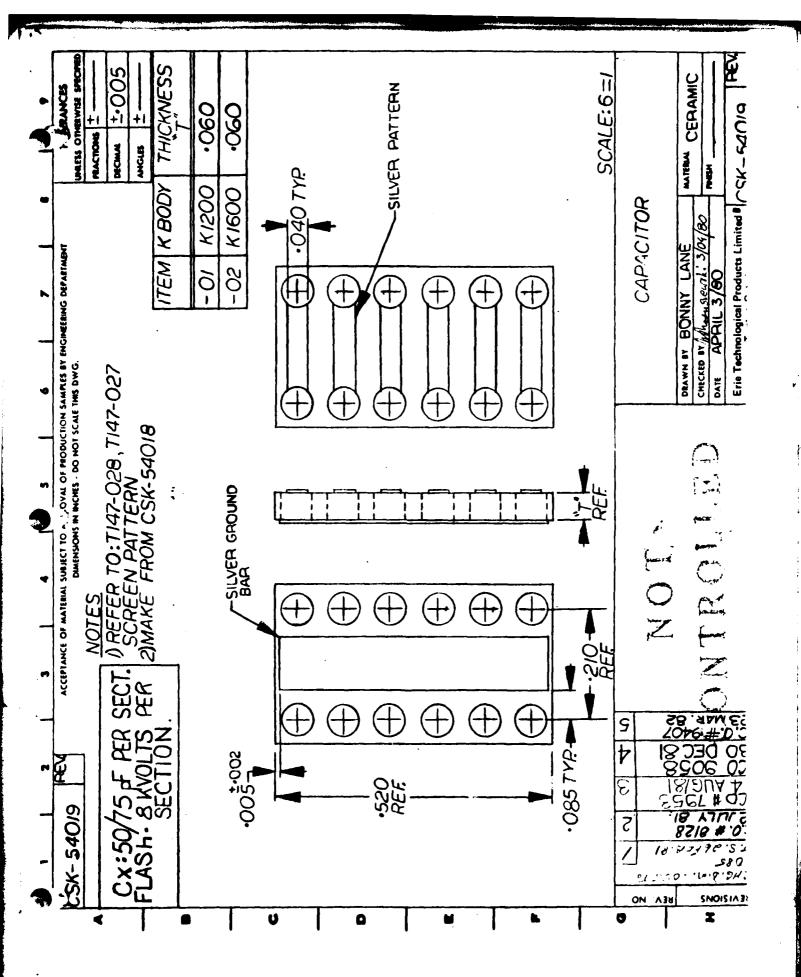
STEP 5

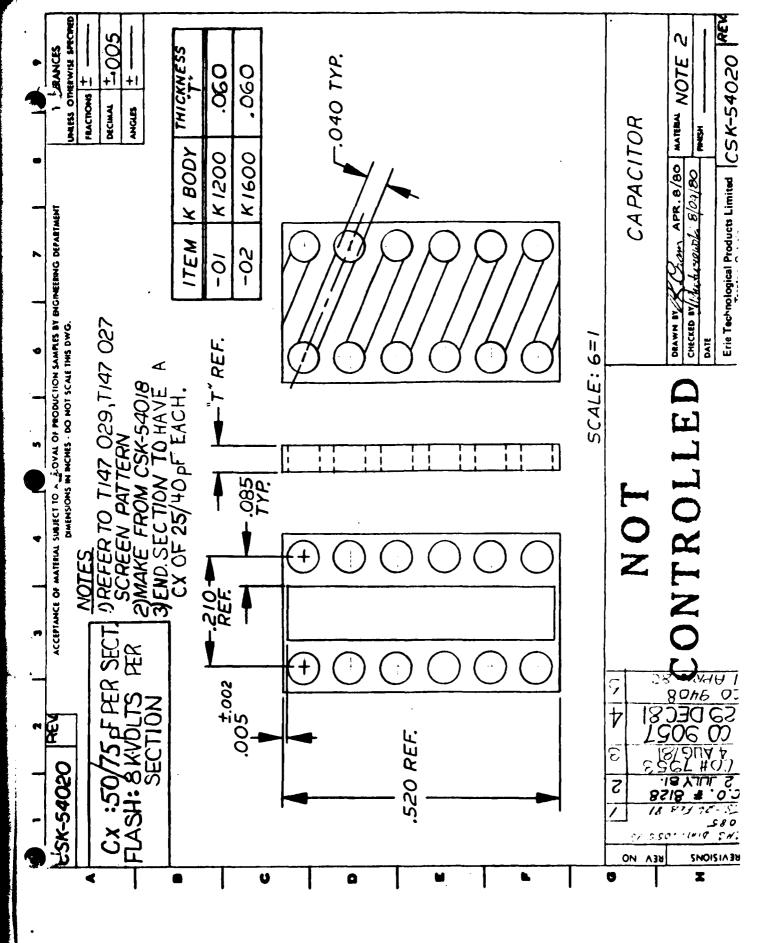


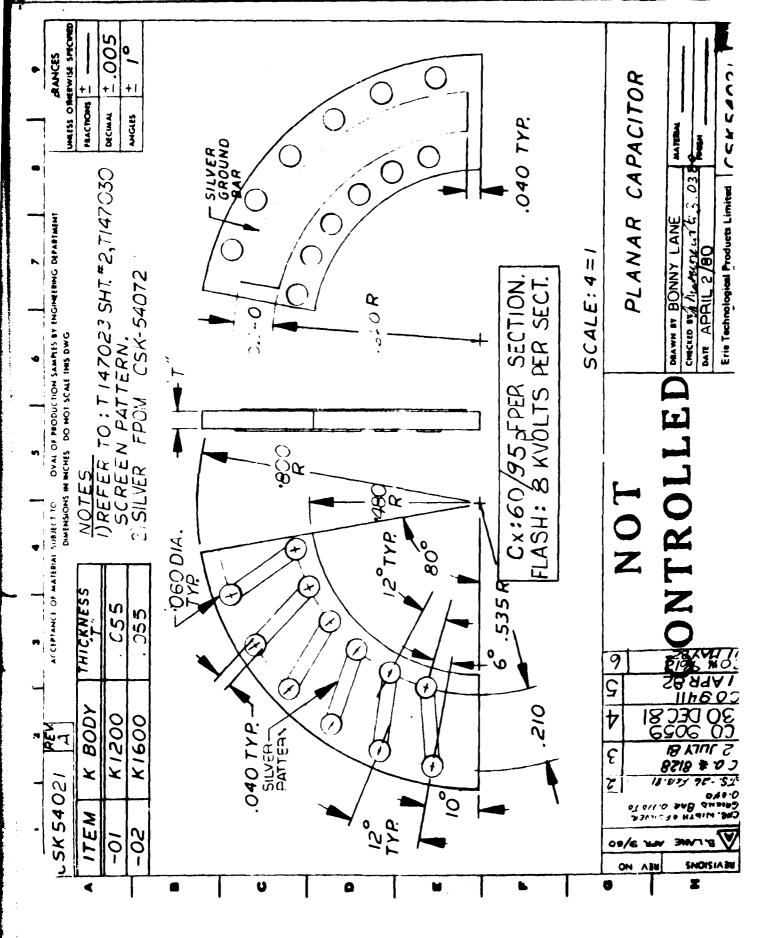
1. LEADS CUT OFF TO EXPOSE SILVER SLUG ON BOTH SIDES. 2. DIODE READY FOR ASSEMBLY.

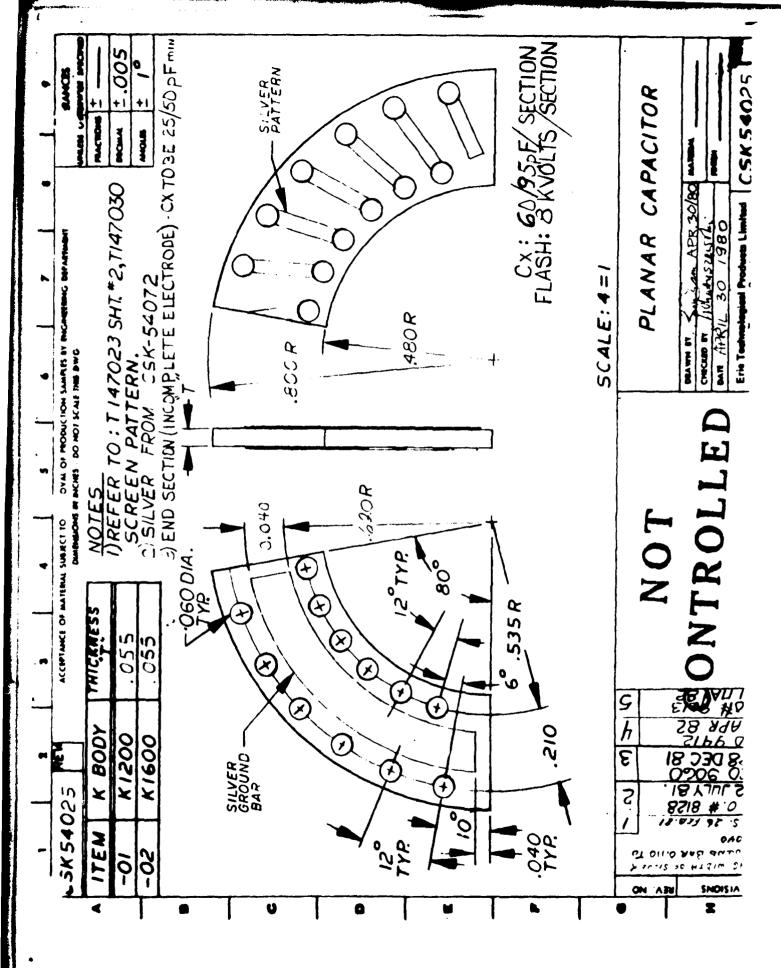
DIODES ARE THEN TESTED FOR: STEP 4

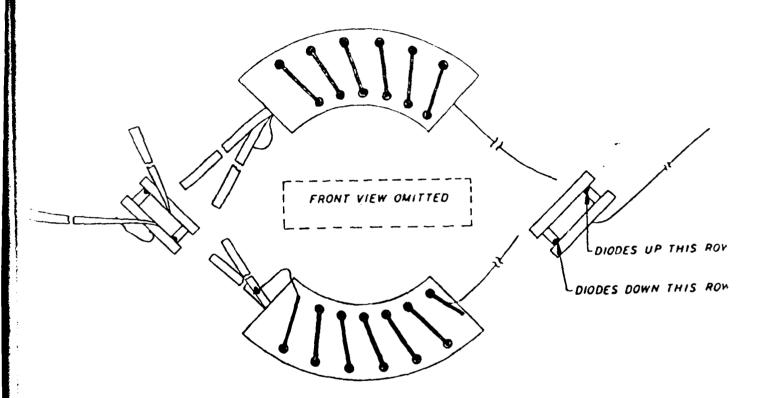
- 1. POLARITY
 2. FORWARD VOLTAGE DROP & JONA.
 MAX 5-0V.
 3. REVERSE LEAKEAGE & 25°C. * 1 K %, ICONA. MAX.
- 4. REVERSE RECOVERY TIME; IF=2-A, IR=2-A, 200 NATIOSECONDS MAX.











TSK 312-00

DATE ILME